

# Direct sequence spread spectrum

In direct sequence (DS) spread spectrum systems, the amplitude of an already modulated signal is amplitude modulated by a very high rate NRZ binary stream of digits. Thus with the original signal

$$s(t) = Ad(t) \cos \omega_0 t$$

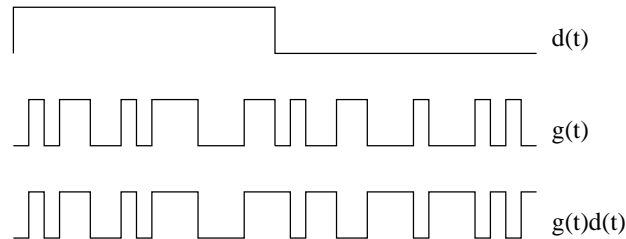
the DS spread spectrum signal is

$$v(t) = g(t)s(t) = Ag(t)d(t) \cos \omega_0 t,$$

where  $g(t)$  is a pseudo-random noise (PN) binary sequence taking on values  $\pm 1$ .

Assume therefore that both  $g(t)$  and  $d(t)$  are binary sequences. The sequence  $g(t)$  is generated in a deterministic manner and is repetitive, but without serious error we can assume that it is truly random. Also, the bit rate  $f_c$  of  $g(t)$  is usually much greater than the bit rate  $f_b$  of  $d(t)$ .  $g(t)$  therefore chops the data into “chips”, and  $f_c$  is called the **chip rate**.

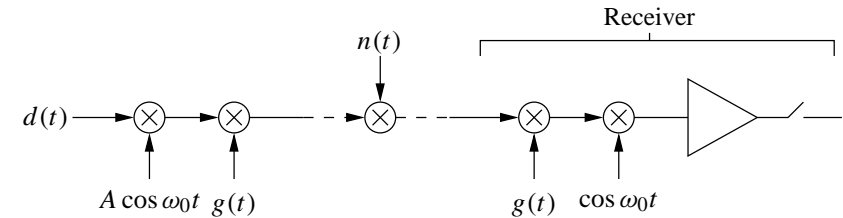
It is standard practice to make the edges of  $g(t)$  and  $d(t)$  coincide, so that each transition in  $d(t)$  coincides with a transition in  $g(t)$ . An example of a waveform, a chipping waveform, and the product waveform is shown below:



The product sequence is seen to be similar to  $g(t)$  — if  $g(t)$  were truly random, then the product sequence would be another random sequence  $g'(t)$  having the same chip rate  $f_c$  as  $g(t)$ . Since the bandwidth of the BPSK signal

$s(t)$  is nominally  $2f_b$  and the bandwidth of the BPSK spread spectrum signal  $v(t)$  is  $2f_c$ , the spectrum has been spread by the ratio  $f_c/f_b$ . The power transmitted by  $s(t)$  and  $v(t)$  is the same, so the power spectral density  $G_s(f)$  is reduced by the factor  $f_b/f_c$ .

A receiver for the DS spread spectrum signal is shown below:



The incoming signal is first multiplied by the waveform  $g(t)$ , and then by the carrier  $\cos \omega_0 t$ . The resulting waveform is then integrated for the duration of the bit, and sampled to yield the data  $d(kT_b)$ . Thus at the receiver it is necessary to regenerate both the sinusoidal carrier of frequency  $\omega_0$  and the PN waveform  $g(t)$ .

One of the primary advantages of spread spectrum signals are their immunity to interfering signals. This is particularly useful in military communications. Suppose a jamming signal of amplitude  $A_J$  is present at the carrier frequency  $\omega_0$ . The input to the receiver then becomes

$$v_I(t) = A_0 d(t) g(t) \cos(\omega_0 t) + A_J \cos(\omega_0 t).$$

At the receiver, after multiplying by the PN signal one obtains

$$A_0 d(t) \cos(\omega_0 t) + A_J g(t) \cos(\omega_0 t).$$

The first term here is a conventional BPSK signal, but the interference in the second term has been spread out in frequency by the action of multiplying by  $g(t)$ . By lowpass filtering the resulting signal the effective power of the interference can be reduced: if  $f_c$  is the chip frequency and  $f_b$  the bit

frequency, then the jammer power at the receiver output is

$$P = \frac{A_J^2}{f_c/f_b}.$$

The spread spectrum receiver has therefore reduced the effect of narrowband jamming by a factor  $f_c/f_b$ . This ratio is called the **processing gain** of the SS receiver.